

Synthesis of an arbitrary ABCD-system with fixed lens positions

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Based on the modified Iwasawa decomposition of a lossless first-order optical system as a cascade of a lens, a magnifier, and a so-called orthosymplectic system, we show how to synthesize an arbitrary **ABCD**-system (with two transverse coordinates) by means of lenses and predetermined sections of free space, so that the lenses are located at fixed positions. © 2006 Optical Society of America
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Any lossless first-order optical system (or **ABCD**-system) can be described by its real symplectic ray transformation matrix¹⁻³ \mathbf{T} , which relates the position \vec{r}_i and direction \vec{p}_i of an incoming ray to the position \vec{r}_o and direction \vec{p}_o of the outgoing ray:

$$\begin{bmatrix} \vec{r}_o \\ \vec{p}_o \end{bmatrix} = \mathbf{T} \begin{bmatrix} \vec{r}_i \\ \vec{p}_i \end{bmatrix} = \begin{bmatrix} \mathbf{A} & \mathbf{B} \\ \mathbf{C} & \mathbf{D} \end{bmatrix} \begin{bmatrix} \vec{r}_i \\ \vec{p}_i \end{bmatrix}. \quad (1)$$

As some well-known one-dimensional examples we mention the matrices

$$\begin{bmatrix} 1 & \lambda z \\ 0 & 1 \end{bmatrix}, \quad \begin{bmatrix} 1 & 0 \\ -1/\lambda f & 1 \end{bmatrix}, \quad \begin{bmatrix} 0 & w^2 \\ -w^{-2} & 0 \end{bmatrix}, \quad (2)$$

see [3, Appendix B.3 and B.4], and in particular⁴

$$\begin{aligned} \mathbf{T}_f(\theta; w) &= \begin{bmatrix} \cos \theta & w^2 \sin \theta \\ -w^{-2} \sin \theta & \cos \theta \end{bmatrix} \\ &= \begin{bmatrix} w & 0 \\ 0 & w^{-1} \end{bmatrix} \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} w^{-1} & 0 \\ 0 & w \end{bmatrix}, \quad (3) \end{aligned}$$

corresponding to a section of free space $\mathcal{S}(z)$ with distance z , a lens $\mathcal{L}(f)$ with focal length f , a Fourier transformer $\mathcal{F}(\pi/2; w)$ with scaling w , and a fractional Fourier transformer^{4,5} $\mathcal{F}(\theta; w)$ with fractional angle θ and scaling w , respectively, acting on light with wavelength λ . Usually we work with normalized variables $w^{-1}r$ and $w p$, so that the fractional Fourier transformer $\mathcal{F}(\theta; w)$ corresponds to a mere rotation in rp -space through an angle θ .

Two commonly used coherent-optical realizations of a (one-dimensional) fractional Fourier transformer $\mathcal{F}(\theta; w)$ have been suggested by Lohmann:⁴ one set-up (a) consisting of a thin (cylindrical) lens $\mathcal{L}(f)$ with focal length f , preceded and followed by two identical distances d of free space $\mathcal{S}(d)$, and another set-up (b) consisting of two identical thin (cylindrical) lenses with focal lengths f , separated by a distance d . In detail, we have for set-up (a), $\mathcal{F}_a(\theta; w) = \mathcal{S}(d)\mathcal{L}(f)\mathcal{S}(d)$,

$$\begin{aligned} \mathbf{T}_f(\theta; w) &= \begin{bmatrix} 1 - d/f & \lambda d(2 - d/f) \\ -(d/f)/\lambda d & 1 - d/f \end{bmatrix}, \\ w^2 \tan(\theta/2) &= \lambda d, \quad (4) \end{aligned}$$

and for set-up (b), $\mathcal{F}_b(\theta; w) = \mathcal{L}(f)\mathcal{S}(d)\mathcal{L}(f)$,

$$\begin{aligned} \mathbf{T}_f(\theta; w) &= \begin{bmatrix} 1 - d/f & \lambda d \\ -(d/f)(2 - d/f)/\lambda d & 1 - d/f \end{bmatrix}, \\ w^2 \sin \theta &= \lambda d, \quad (5) \end{aligned}$$

which are equivalent to Eq. (3) for $\sin^2(\theta/2) = d/2f$. Note that in these set-ups, with $0 \leq d/2f \leq 1$, the fractional angle θ is restricted to the interval $0 \leq \theta \leq \pi$, and that for θ outside that interval we have to perform an additional reversion of the coordinates (or use a cascade of two such fractional Fourier transform set-ups). Two crossed one-dimensional fractional Fourier transformers, with different fractional angles $\theta_{x,y}$ and different scaling factors $w_{x,y}$, now lead to a two-dimensional, separable fractional Fourier transformer $\mathcal{F}(\theta_x, \theta_y; w_x, w_y)$, with ray transformation matrix $\mathbf{T}_f(\theta_x, \theta_y; w_x, w_y)$.

If d is a *fixed* distance in Lohmann's set-ups, problems arise when $\theta \approx 0$ or $\theta \approx \pi$, in which case w^2 may tend to 0 or ∞ . These problems can be avoided if we restrict θ to a smaller range around $\pi/2$, for instance $-\pi/N \leq \theta - \pi/2 \leq \pi/N$ with $N > 2$. If we then need a fractional Fourier transformer $\mathcal{F}(\theta; w)$ with the fractional angle θ in the full range of length 2π (hence $-\pi \leq \theta - N\pi/2 \leq \pi$), we simply use a cascade of N such reduced-angle transformers, $\mathcal{F}(\theta; w) = \mathcal{F}^N(\theta/N; w)$, while at the same time avoiding a coordinate reversion.

When we work with normalized coordinates, we will use lower-case characters to denote the resulting normalized matrices. So, with \mathbf{W} a diagonal scaling matrix (to be determined later), we have

$$\begin{bmatrix} \mathbf{W}^{-1} & \mathbf{0} \\ \mathbf{0} & \mathbf{W} \end{bmatrix} \begin{bmatrix} \vec{r}_o \\ \vec{p}_o \end{bmatrix} = \begin{bmatrix} \mathbf{a} & \mathbf{b} \\ \mathbf{c} & \mathbf{d} \end{bmatrix} \begin{bmatrix} \mathbf{W}^{-1} & \mathbf{0} \\ \mathbf{0} & \mathbf{W} \end{bmatrix} \begin{bmatrix} \vec{r}_i \\ \vec{p}_i \end{bmatrix}, \quad (6)$$

where the **abcd**-matrix is the normalized version of the **ABCD**-matrix.

If the ray transformation matrix is not only real symplectic but also orthogonal, we call the system orthosymplectic.⁶ The ray transformation matrix of such

an orthosymplectic system takes the general form

$$\begin{bmatrix} \mathbf{W} & \mathbf{0} \\ \mathbf{0} & \mathbf{W}^{-1} \end{bmatrix} \begin{bmatrix} \mathbf{x} & \mathbf{y} \\ -\mathbf{y} & \mathbf{x} \end{bmatrix} \begin{bmatrix} \mathbf{W}^{-1} & \mathbf{0} \\ \mathbf{0} & \mathbf{W} \end{bmatrix}, \quad (7)$$

where \mathbf{W} is again the diagonal scaling matrix and where the two matrices \mathbf{x} and \mathbf{y} can be combined into a complex matrix $\mathbf{u} = \mathbf{x} + i\mathbf{y}$ that is unitary: $\mathbf{u}^\dagger = \mathbf{u}^{-1}$, with \mathbf{u}^\dagger the transposed and complex conjugated version of \mathbf{u} . In the two-dimensional case, with $\vec{r} = (r_x, r_y)^t$ and $\vec{p} = (p_x, p_y)^t$, basic members of the orthosymplectic class that we will use in this paper, are the two-dimensional separable fractional Fourier transformer $\mathcal{F}(\theta_x, \theta_y; w_x, w_y)$ and the rotator $\mathcal{R}(\theta)$ (also called image gyrator⁷), with ray transformation matrices

$$\mathbf{t}_f(\theta_x, \theta_y) = \begin{bmatrix} \cos \theta_x & 0 & \sin \theta_x & 0 \\ 0 & \cos \theta_y & 0 & \sin \theta_y \\ -\sin \theta_x & 0 & \cos \theta_x & 0 \\ 0 & -\sin \theta_y & 0 & \cos \theta_y \end{bmatrix}, \quad (8)$$

$$\mathbf{t}_r(\theta) = \begin{bmatrix} \cos \theta & \sin \theta & 0 & 0 \\ -\sin \theta & \cos \theta & 0 & 0 \\ 0 & 0 & \cos \theta & \sin \theta \\ 0 & 0 & -\sin \theta & \cos \theta \end{bmatrix}, \quad (9)$$

and unitary representations

$$\mathbf{u}_f(\theta_x, \theta_y) = \begin{bmatrix} \exp(i\theta_x) & 0 \\ 0 & \exp(i\theta_y) \end{bmatrix}, \quad (10)$$

$$\mathbf{u}_r(\theta) = \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix}, \quad (11)$$

see also [6, Section 10.3.2, Eq. (10.31)] and [7, Eqs. (49)], respectively. We remark that a rotator with rotation angle θ produces a rotation through the angle θ , both for the space variables (r_x, r_y) and the direction variables (p_x, p_y) .

We now represent the normalized symplectic **abcd**-matrix by means of its modified Iwasawa decomposition.⁸ In particular we have [6, Sections 9.5 and 10.2]

$$\begin{bmatrix} \mathbf{a} & \mathbf{b} \\ \mathbf{c} & \mathbf{d} \end{bmatrix} = \begin{bmatrix} \mathbf{I} & \mathbf{0} \\ -\mathbf{g} & \mathbf{I} \end{bmatrix} \begin{bmatrix} \mathbf{s} & \mathbf{0} \\ \mathbf{0} & \mathbf{s}^{-1} \end{bmatrix} \begin{bmatrix} \mathbf{x} & \mathbf{y} \\ -\mathbf{y} & \mathbf{x} \end{bmatrix}, \quad (12)$$

where the first matrix corresponds to a lens described by the symmetric matrix $\mathbf{G} = \mathbf{W}^{-1}\mathbf{g}\mathbf{W}^{-1}$ with $\mathbf{g} = -(\mathbf{c}\mathbf{a}^t + \mathbf{d}\mathbf{b}^t)(\mathbf{a}\mathbf{a}^t + \mathbf{b}\mathbf{b}^t)^{-1}$, the second matrix corresponds to a magnifier described by the positive-definite symmetric matrix $\mathbf{S} = \mathbf{W}\mathbf{s}\mathbf{W}^{-1}$ with $\mathbf{s} = (\mathbf{a}\mathbf{a}^t + \mathbf{b}\mathbf{b}^t)^{1/2}$, and the third matrix represents an orthosymplectic system described by the unitary matrix $\mathbf{u} = \mathbf{x} + i\mathbf{y} = (\mathbf{a}\mathbf{a}^t + \mathbf{b}\mathbf{b}^t)^{-1/2}(\mathbf{a} + i\mathbf{b})$.

Based on the modified Iwasawa decomposition, we will now derive how – in the two-dimensional case – an arbitrary **ABCD**-system can be synthesized with fixed lens positions. We remark that (without fixed lens positions) the one-dimensional case has been treated before,⁹ while an existence proof (without presenting an explicit synthesis method) has been given for the two-dimensional case.² We recall that we have $\vec{r} = (r_x, r_y)^t$,

that the 4×4 symplectic ray transformation matrix \mathbf{T} has 10 degrees of freedom, that the matrices \mathbf{G} , \mathbf{g} , \mathbf{S} , \mathbf{s} , \mathbf{x} , and \mathbf{y} are 2×2 matrices, and that the 2×2 scaling matrix \mathbf{W} still has to be determined. We start with the orthosymplectic subsystem.

It can be shown¹⁰ that in the two-dimensional case, the orthosymplectic subsystem in the modified Iwasawa decomposition (12), described by the unitary matrix $\mathbf{u} = \mathbf{x} + i\mathbf{y}$, can be realized as a separable fractional Fourier transformer $\mathcal{F}(\gamma_x, \gamma_y)$, see Eqs. (8) and (10), embedded in between two rotators $\mathcal{R}(\alpha)$ and $\mathcal{R}(\beta)$, see Eqs. (9) and (11): $\mathcal{R}(\beta)\mathcal{F}(\gamma_x, \gamma_y)\mathcal{R}(\alpha)$. We thus have $\mathbf{u} = \mathbf{u}_r(\beta)\mathbf{u}_f(\gamma_x, \gamma_y)\mathbf{u}_r(\alpha)$, see also [6, Eq. (10.32)]. The fractional angles γ_x and γ_y follow from the relations¹⁰ $\exp[i(\gamma_x + \gamma_y)] = \det \mathbf{u}$ and $\cos(\gamma_x - \gamma_y) = \det \mathbf{x} + \det \mathbf{y}$, where the π phase ambiguity can be avoided by choosing $0 \leq \gamma_x - \gamma_y < \pi$. The rotation angles α and β can then be determined from the elements of the matrices \mathbf{x} and \mathbf{y} .¹⁰

While the rotators $\mathcal{R}(\alpha)$ and $\mathcal{R}(\beta)$ can be dealt with by simply defining rotated coordinate systems, the separable fractional Fourier transformer $\mathcal{F}(\gamma_x, \gamma_y)$ (with different fractional angles γ_x and γ_y in the two perpendicular directions) can be realized, for instance, by (cascades of) Lohmann's set-ups $\mathcal{F}_a = \mathcal{S}\mathcal{L}\mathcal{S}$ or $\mathcal{F}_b = \mathcal{L}\mathcal{S}\mathcal{L}$, possibly combined with a reversion of the coordinates, as described before. We then have combinations of two crossed cylindrical lenses (with different focal lengths f_x and f_y) combined with fixed distances d of free space, with proper rotations of the coordinate systems before and after the separable fractional Fourier transformer. The two fractional angles and the two rotation angles constitute four degrees of freedom.

It is important to note that for any separable fractional Fourier transformer that we want to synthesize, the distance d can be chosen to be *constant*, which is exactly what we will do; the two focal distances f_x and f_y are then further determined by γ_x and γ_y , respectively. The fractional Fourier transformer determines also the scaling factors $w_{x,y}$ (depending on $\sqrt{\lambda d}$ and $\gamma_{x,y}$), so that the scaling matrix \mathbf{W} is now known.

The lens in the modified Iwasawa decomposition (12) is described by the symmetric matrix $\mathbf{G} = \mathbf{W}^{-1}\mathbf{g}\mathbf{W}^{-1}$, which can be decomposed as

$$\mathbf{G} = \begin{bmatrix} g_{11} & g_{12} \\ g_{12} & g_{22} \end{bmatrix} = \mathbf{u}_r(\varphi_g) \begin{bmatrix} g_1 & 0 \\ 0 & g_2 \end{bmatrix} \mathbf{u}_r(-\varphi_g), \quad (13)$$

where $g_{1,2} = (g_{11} + g_{22})/2 \pm \sqrt{[(g_{11} - g_{22})/2]^2 + g_{12}^2}$ and $\tan \varphi_g = (g_{11} - g_1)/g_{12} = g_{12}/(g_{22} - g_1) = g_{12}/(g_2 - g_{11}) = (g_2 - g_{22})/g_{12}$; see also [6, Section 10.2.1, Lenses]. This decomposition shows a possible realization of the two-dimensional (anamorphic) lens as a combination of two crossed cylindrical lenses whose focal lengths read $1/\lambda g_1$ and $1/\lambda g_2$, and which is oriented at an angle φ_g : $\mathcal{R}(\varphi_g)\mathcal{L}(1/\lambda g_1, 1/\lambda g_2)\mathcal{R}(-\varphi_g)$. The two focal lengths and the orientation angle constitute three degrees of freedom.

The magnifier in the modified Iwasawa decomposition (12) is described by the positive-definite symmetric

matrix $\mathbf{S} = \mathbf{W}\mathbf{s}\mathbf{W}^{-1}$, which can again be decomposed as

$$\mathbf{S} = \begin{bmatrix} s_{11} & s_{12} \\ s_{12} & s_{22} \end{bmatrix} = \mathbf{u}_r(\varphi_s) \begin{bmatrix} s_1 & 0 \\ 0 & s_2 \end{bmatrix} \mathbf{u}_r(-\varphi_s), \quad (14)$$

cf. Eq. (13); see also [6, Section 10.2.2, Magnifiers]. Note that $s_1 s_2 = \det \mathbf{s} > 0$ and $s_1 + s_2 = \text{Tr } \mathbf{s} > 0$. The two-dimensional (anamorphic) magnifier can thus be realized as a combination of two crossed one-dimensional magnifiers whose magnification factors are defined by s_1 and s_2 , and which is oriented at an angle φ_s .

A one-dimensional magnifier (with reversion) can easily be realized by means of an ideal imaging system built around a thin (cylindrical) lens with focal distance f_o . The input plane of this system is located a distance d_o before the lens, whereas its output plane is located a distance z_o behind the lens. To get ideal imaging, we have of course the condition $1/d_o + 1/z_o = 1/f_o$, and the magnification is then $s = z_o/d_o$; to avoid the occurrence of a small value of f_o , we require that the magnification s is not too small. To compensate for an unwanted phase factor, we use a thin (cylindrical) phase-correcting lens with focal distance $z_o - f_o$ in the output plane. In detail we thus have $\mathcal{L}(z_o - f_o)\mathcal{S}(z_o)\mathcal{L}(f_o)\mathcal{S}(d_o)$:

$$\begin{aligned} & \begin{bmatrix} 1 & 0 \\ -1/\lambda(z_o - f_o) & 1 \end{bmatrix} \begin{bmatrix} 1 & \lambda z_o \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ -1/\lambda f_o & 1 \end{bmatrix} \begin{bmatrix} 1 & \lambda d_o \\ 0 & 1 \end{bmatrix} \\ & = - \begin{bmatrix} (z_o - f_o)/f_o & 0 \\ 0 & f_o/(z_o - f_o) \end{bmatrix} \equiv - \begin{bmatrix} s & 0 \\ 0 & s^{-1} \end{bmatrix}. \quad (15) \end{aligned}$$

Note that the overall minus sign corresponds to reversion; we will automatically compensate for that later.

Two crossed one-dimensional magnifiers, with different magnifications $s_1 = z_1/d_1$ and $s_2 = z_2/d_2$ in the two perpendicular directions, and with $z_1 + d_1 = z_2 + d_2$, would lead to a two-dimensional, separable magnifier. The two magnification factors and the orientation angle constitute again three degrees of freedom.

To obtain fixed lens positions in the magnifier (and thus choosing $d_1 = d_2 = d_o$), we remark that a (one-dimensional) section of free space $z_o = s d_o$ can be synthesized by a lens embedded in between two Fourier transformers, $\mathcal{S}(z_o) = \mathcal{F}(\pi/2; w)\mathcal{L}(f)\mathcal{F}(\pi/2; w)$:

$$\begin{aligned} & \begin{bmatrix} 0 & w^2 \\ -w^{-2} & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ -1/\lambda f & 1 \end{bmatrix} \begin{bmatrix} 0 & w^2 \\ -w^{-2} & 0 \end{bmatrix} \\ & = - \begin{bmatrix} 1 & w^4/\lambda f \\ 0 & 1 \end{bmatrix} \equiv - \begin{bmatrix} 1 & \lambda z_o \\ 0 & 1 \end{bmatrix}. \quad (16) \end{aligned}$$

The distance z_o , the focal distance f of the lens, and the scaling w of the Fourier transformers are related as $f = w^4/\lambda^2 z_o$; to avoid a small value of f , we now require also that s is not too large. Note that the coordinate reversion that corresponds to the overall minus sign in Eq. (16) compensates the reversion that we encountered before in Eq. (15). A (one-dimensional) magnifier with magnification $s = z_o/d_o$ can thus be synthesized by a cascade of a section of free space with *constant* distance d_o , a

lens with focal distance $f_o = (1/d_o + 1/z_o)^{-1}$, a lens with focal distance $w^4/\lambda^2 z_o$ embedded in between two Fourier transformers with scaling w , and a phase-correcting lens with focal distance $z_o - f_o$: $\mathcal{L}(z_o - f_o)\mathcal{F}(\pi/2; w)\mathcal{L}(w^4/\lambda^2 z_o)\mathcal{F}(\pi/2; w)\mathcal{L}(f_o)\mathcal{S}(d_o)$.

The final two-dimensional cascade then takes the form

$$\begin{aligned} & \mathcal{R}(\varphi_g)\mathcal{L}(1/\lambda g_1, 1/\lambda g_2)\mathcal{R}(-\varphi_g)\mathcal{R}(\varphi_s)\mathcal{L}(z_1 - f_1, z_2 - f_2) \\ & \times \mathcal{F}_b(\pi/2; w)\mathcal{L}(w^4/\lambda^2 z_1, w^4/\lambda^2 z_2)\mathcal{F}_b(\pi/2; w)\mathcal{L}(f_1, f_2) \\ & \times \mathcal{S}(d_o)\mathcal{R}(-\varphi_s)\mathcal{R}(\beta)\mathcal{F}(\gamma_x, \gamma_y; w_x, w_y)\mathcal{R}(\alpha). \quad (17) \end{aligned}$$

Besides the constant distance d_o , sections of free space appear only inside the (fractional) Fourier transformers and can be chosen to be constant, resulting in fixed positions of the lenses. Of course, rotators \mathcal{R} and sections of free space \mathcal{S} commute, and adjacent rotators \mathcal{R} and lenses \mathcal{L} can be combined into one single (anamorphic) lens with a proper orientation, in which case the number of lenses (and predetermined sections of free space) in the final cascade (17), $\mathcal{R}\mathcal{L}\mathcal{R}\mathcal{R}\mathcal{L}\mathcal{L}\mathcal{S}\mathcal{L}\mathcal{L}\mathcal{S}\mathcal{L}\mathcal{L}\mathcal{S}\mathcal{R}\mathcal{R}\mathcal{F}\mathcal{R}$, reduces to three plus the number of lenses used to realize the fractional Fourier transformer $\mathcal{F}(\gamma_x, \gamma_y; w_x, w_y)$.

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