

# Synthesis of an arbitrary ABCD-system, based on the modified Iwasawa decomposition



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## Lossless first-order optical systems

A lossless first-order optical system (or **ABCD** system) is described by its **symplectic ray transformation matrix**. After normalizing this **ABCD** matrix,

$$\begin{bmatrix} \mathbf{A} & \mathbf{B} \\ \mathbf{C} & \mathbf{D} \end{bmatrix} = \begin{bmatrix} \mathbf{w} & \mathbf{0} \\ \mathbf{0} & \mathbf{w}^{-1} \end{bmatrix} \begin{bmatrix} \mathbf{a} & \mathbf{b} \\ \mathbf{c} & \mathbf{d} \end{bmatrix} \begin{bmatrix} \mathbf{w}^{-1} & \mathbf{0} \\ \mathbf{0} & \mathbf{w} \end{bmatrix}, \quad \mathbf{w} = \begin{bmatrix} w_x & 0 \\ 0 & w_y \end{bmatrix}$$

with  $w_x, w_y > 0$ , the normalized **abcd** matrix can be decomposed into the so-called **modified Iwasawa decomposition**

$$\begin{bmatrix} \mathbf{a} & \mathbf{b} \\ \mathbf{c} & \mathbf{d} \end{bmatrix} = \begin{bmatrix} \mathbf{I} & \mathbf{0} \\ -\mathbf{g} & \mathbf{I} \end{bmatrix} \begin{bmatrix} \mathbf{s} & \mathbf{0} \\ \mathbf{0} & \mathbf{s}^{-1} \end{bmatrix} \begin{bmatrix} \mathbf{x} & \mathbf{y} \\ -\mathbf{y} & \mathbf{x} \end{bmatrix} \equiv \mathcal{L}(\mathbf{g}) \mathcal{M}(\mathbf{s}) \mathcal{O}(\mathbf{x} + i\mathbf{y}),$$

where the **anamorphic lens**  $\mathcal{L}(\mathbf{g})$  (e.g., two crossed cylindrical lenses, oriented at the appropriate angle) is described by the symmetric matrix  $\mathbf{g} = -(\mathbf{c}\mathbf{a}^t + \mathbf{d}\mathbf{b}^t)(\mathbf{a}\mathbf{a}^t + \mathbf{b}\mathbf{b}^t)^{-1}$ , the **separable magnifier**  $\mathcal{M}(\mathbf{s})$  (using, e.g., two crossed cylindrical lenses with proper orientation again) by the positive-definite symmetric matrix  $\mathbf{s} = (\mathbf{a}\mathbf{a}^t + \mathbf{b}\mathbf{b}^t)^{1/2}$ , and the **orthosymplectic system**  $\mathcal{O}(\mathbf{u})$  by the unitary matrix  $\mathbf{u} = \mathbf{x} + i\mathbf{y} = (\mathbf{a}\mathbf{a}^t + \mathbf{b}\mathbf{b}^t)^{-1/2}(\mathbf{a} + i\mathbf{b})$ .  $\mathcal{O}(\mathbf{u})$  can be realized in many ways, for instance as a **separable fractional Fourier transformer** (with different fractional angles in the two perpendicular directions) embedded in between two **rotators** (with different rotation angles):  $\mathcal{R}(\beta) \mathcal{F}(\gamma_x, \gamma_y) \mathcal{R}(\alpha)$ .

## One-dimensional case

The basic  $2 \times 2$  ray transformation matrices

$$\begin{bmatrix} 1 & \lambda z \\ 0 & 1 \end{bmatrix}, \quad \begin{bmatrix} 1 & 0 \\ -1/\lambda f & 1 \end{bmatrix}, \quad \begin{bmatrix} \cos \gamma & w^2 \sin \gamma \\ -w^{-2} \sin \gamma & \cos \gamma \end{bmatrix}$$

correspond to a section of **free space**  $\mathcal{S}(z)$  with distance  $z$ , a **cylindrical lens**  $\mathcal{L}(f)$  with focal length  $f$ , and a **fractional Fourier transformer**  $\mathcal{F}(\gamma; w)$  with fractional angle  $\gamma$  and scaling  $w$ , respectively, acting on light with wavelength  $\lambda$ .

The Iwasawa decomposition leads to the actual realization

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ -gw^{-2} & 1 \end{bmatrix} \begin{bmatrix} s & 0 \\ 0 & s^{-1} \end{bmatrix} \begin{bmatrix} \cos \gamma & w^2 \sin \gamma \\ -w^{-2} \sin \gamma & \cos \gamma \end{bmatrix}$$

and in **operator notation**  $\mathcal{L}(w^2/\lambda g) \mathcal{M}(s) \mathcal{F}(\gamma; w)$ .

A **magnifier**  $\mathcal{M}(s)$  (with reversion) can be realized as

$$\mathcal{L}(z_o - f_o) \mathcal{S}(z_o) \mathcal{L}(f_o) \mathcal{S}(d_o)$$

with  $1/d_o + 1/z_o = 1/f_o$  and  $s = z_o/d_o$ .

For the **fractional Fourier transformer**  $\mathcal{F}(\gamma; w)$  we may use one of the two Lohmann setups for which  $\sin^2(\gamma/2) = \tilde{d}/2f$ :

- (a)  $\mathcal{F}_a(\gamma; \tilde{w}) = \mathcal{S}(\tilde{d}) \mathcal{L}(\tilde{f}) \mathcal{S}(\tilde{d})$  with  $\tilde{w}^2 \tan(\gamma/2) = \lambda \tilde{d}$
- (b)  $\mathcal{F}_b(\gamma; \tilde{w}) = \mathcal{L}(\tilde{f}) \mathcal{S}(\tilde{d}) \mathcal{L}(\tilde{f})$  with  $\tilde{w}^2 \sin \gamma = \lambda \tilde{d}$

$$\mathcal{M}(w\tilde{w}^{-1}) \mathcal{F}(\gamma; \tilde{w}) \mathcal{M}(\tilde{w}w^{-1})$$

Note the **scale adapter**  $\mathcal{M}(w\tilde{w}^{-1})$  and the freedom for  $\tilde{w}$ .

The **final one-dimensional cascade**, using setup (a), leads to

$$\mathcal{L}(w^2/\lambda g) \mathcal{L}(z_o - f_o) \mathcal{S}(z_o) \mathcal{L}(f_o) \mathcal{S}(d_o) \mathcal{S}(\tilde{d}) \mathcal{L}(\tilde{f}) \mathcal{S}(\tilde{d})$$

with three lenses and three sections of free space; note that the final lens  $\mathcal{L}(f)$  with  $1/f = \lambda g/w^2 + 1/(z_o - f_o)$  takes also care of the phase correction that is required for the magnifier.

## Two-dimensional case

In the two-dimensional case, two new elements will enter the description: a **rotator**  $\mathcal{R}(\varphi)$  and a **scaling magnifier**  $\mathcal{M}_o = \mathcal{M}(w_x^{1/2} w_y^{-1/2}, w_x^{-1/2} w_y^{1/2})$  (necessary if  $w_x \neq w_y$ ), with

$$\mathbf{u}_r(\varphi) = \begin{bmatrix} \cos \varphi & \sin \varphi \\ -\sin \varphi & \cos \varphi \end{bmatrix}, \quad \mathbf{s}_o = \begin{bmatrix} w_x^{1/2} w_y^{-1/2} & 0 \\ 0 & w_x^{-1/2} w_y^{1/2} \end{bmatrix}.$$

The matrix  $\mathbf{G}$  of the **anamorphic lens** can be written as

$$\mathbf{G} = \mathbf{w}^{-1} \mathbf{g} \mathbf{w}^{-1} = \begin{bmatrix} g_{11} & g_{12} \\ g_{12} & g_{22} \end{bmatrix} = \mathbf{u}_r(\varphi_g) \begin{bmatrix} g_1 & 0 \\ 0 & g_2 \end{bmatrix} \mathbf{u}_r(-\varphi_g)$$

and leads to a combination of two crossed cylindrical lenses whose focal lengths read  $1/\lambda g_1$  and  $1/\lambda g_2$ , and which is oriented at an angle  $\varphi_g$ :  $\mathcal{R}(\varphi_g) \mathcal{L}(1/\lambda g_1, 1/\lambda g_2) \mathcal{R}(-\varphi_g)$ .

For the **separable magnifier** we have  $\mathbf{w} \mathbf{s} \mathbf{w}^{-1} = \mathbf{s}_o \mathbf{s} \mathbf{s}_o^{-1}$ , which leads to

$$\mathcal{M}_o \mathcal{R}(\varphi_s) \mathcal{M}(s_1, s_2) \mathcal{R}(-\varphi_s) \mathcal{M}_o^{-1}.$$

Two crossed 1D magnifiers, with different magnifications  $s_1 = z_1/d_1$  and  $s_2 = z_2/d_2$  in the two perpendicular directions, and with  $z_1 + d_1 = z_2 + d_2$ , lead to a separable magnifier.

We also have  $\mathbf{w} \mathbf{u}_r(\varphi) \mathbf{w}^{-1} = \mathbf{s}_o \mathbf{u}_r(\varphi) \mathbf{s}_o^{-1}$ , so that a **rotator** embedded in between scaling magnifiers leads to

$$\mathcal{M}_o \mathcal{R}(\varphi) \mathcal{M}_o^{-1}.$$

Finally, the **separable fractional Fourier transformer**

$$\begin{bmatrix} \cos \gamma_x & 0 & w_x^2 \sin \gamma_x & 0 \\ 0 & \cos \gamma_y & 0 & w_y^2 \sin \gamma_y \\ -w_x^{-2} \sin \gamma_x & 0 & \cos \gamma_x & 0 \\ 0 & -w_y^{-2} \sin \gamma_y & 0 & \cos \gamma_y \end{bmatrix}$$

is simply a concatenation of two 1D fractional Fourier transformers. And like before, we have

$$\mathcal{M}(w_x \tilde{w}_x^{-1}, w_y \tilde{w}_y^{-1}) \mathcal{F}(\gamma_x, \gamma_y; \tilde{w}_x, \tilde{w}_y) \mathcal{M}(\tilde{w}_x w_x^{-1}, \tilde{w}_y w_y^{-1}).$$

From a practical point of view we may require that the input and output planes of the separable fractional Fourier transformer for the  $x$  and the  $y$  coordinates coincide:  $\tilde{d}_x = \tilde{d}_y = \tilde{d}$ . This leads to  $\tilde{w}_x^2 \tan(\gamma_x/2) = \tilde{w}_y^2 \tan(\gamma_y/2)$  for setup (a) and to  $\tilde{w}_x^2 \sin \gamma_x = \tilde{w}_y^2 \sin \gamma_y$  for setup (b), where we have tacitly assumed that  $\gamma_{x,y} \neq 0$ . **We thus need freedom for  $\tilde{w}_{x,y}$ .**

After choosing  $w_x = w_y = w$ , the **final cascade** takes the form

$$\mathcal{R}(\varphi_g) \mathcal{L}(1/\lambda g_1, 1/\lambda g_2) \mathcal{R}(\varphi_s - \varphi_g) \mathcal{M}(s_1, s_2) \mathcal{R}(\beta - \varphi_s) \mathcal{M}(w\tilde{w}_x^{-1}, w\tilde{w}_y^{-1}) \mathcal{F}(\gamma_x, \gamma_y; \tilde{w}_x, \tilde{w}_y) \mathcal{M}(\tilde{w}_x w^{-1}, \tilde{w}_y w^{-1}) \mathcal{R}(\alpha).$$

The number of cylindrical lenses that we need, equals ten: two lenses for the anamorphic lens (which at the same time take care of the phase corrections for the separable magnifier); two lenses to realize the separable magnifier; two lenses for the separable fractional Fourier transformer; and two lenses for each of the scale adapters that embed the fractional Fourier transformer.